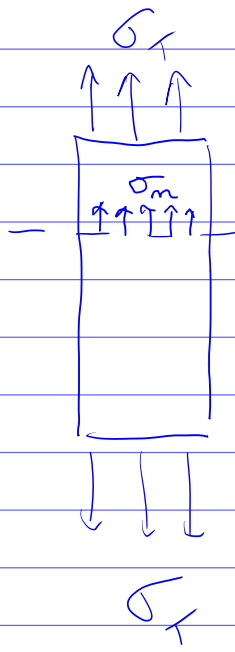


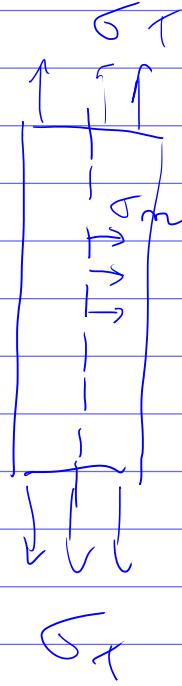
# 1. Chapitre Contraintes

- 1) Existence du tenseur des contraintes
- 2) Equation d'équilibre
- 3) Symétrie
- 4) Commentaires / exemples

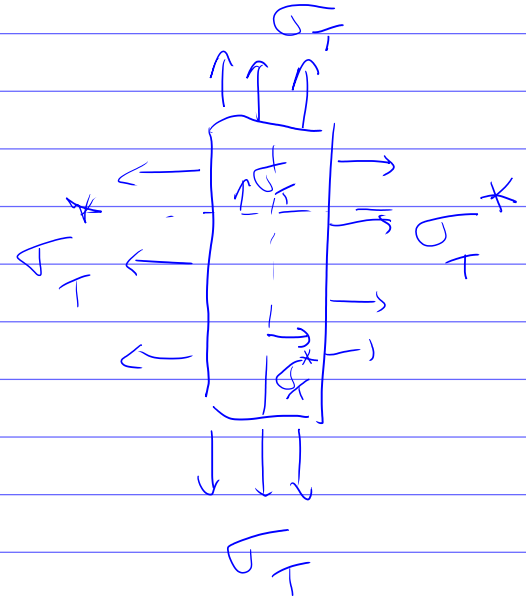
$\Rightarrow$  depends on  $\vec{n}$  (example)



$$\sigma_n = \sigma_T$$

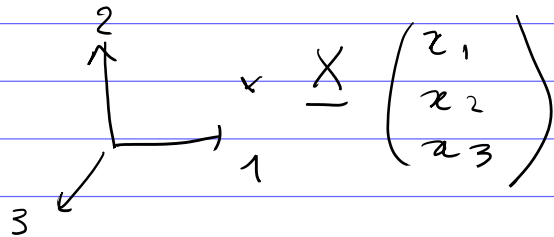


$$\sigma_n = 0$$



1) Existence

\* Preamble

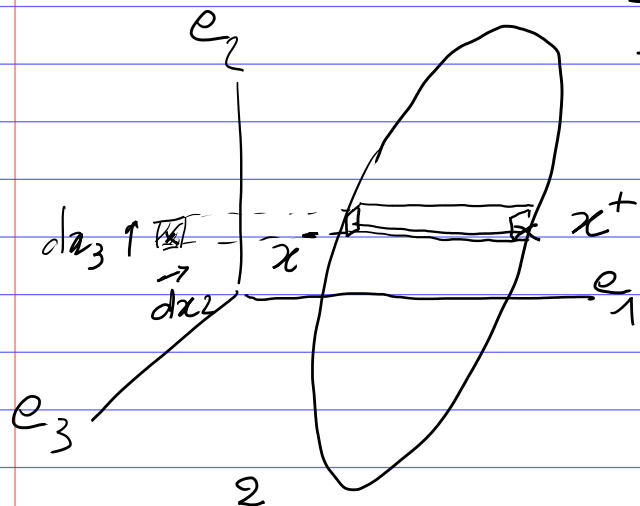


Supposons  $f: x_1 \mapsto f(x_1)$

also

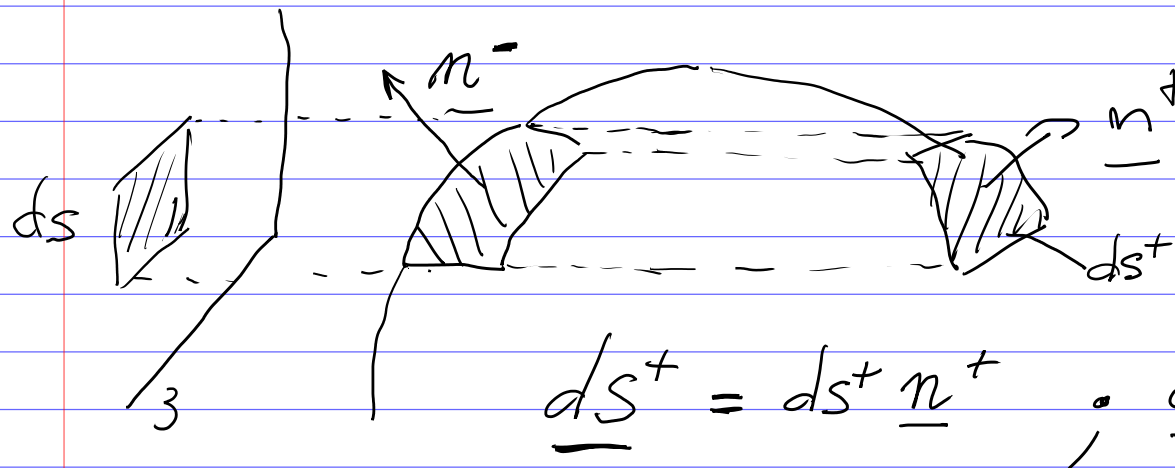
$\iint_{\Omega} \frac{df}{dx_1} dv = \iint_{\partial\Omega} f n_1 ds$

Démo :



$$I = \iiint_V \frac{dA}{dn_1} dv = \iint_{x_2, x_3} \left( \int_{x_1} \frac{dA}{dn_1} dx_1 \right) dx_2 dx_3$$

$$= f(x_1^+) - f(x_1^-)$$



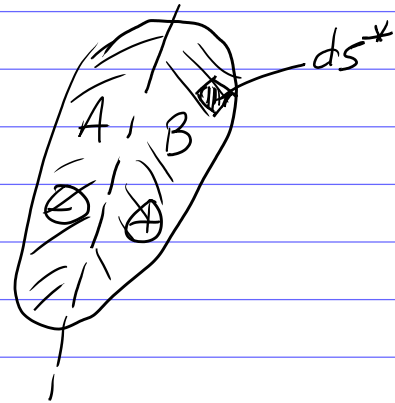
Req: Surface projetée de  $\underline{ds}$  dans la direction  $\underline{n}$  est égale à  $\underline{ds} \cdot \underline{n}$

$$\underline{ds}^+ = ds^+ \underline{n}^+ ; \quad \underline{ds}^- = ds^- \underline{n}^-$$

$$ds = \underline{ds}^+ \cdot \underline{e}_1 = \underline{ds}^- \cdot \underline{e}_1$$

$$I = \iint_{x_2, x_3} f(x^+) \underline{n}^+ \cdot \underline{e}_1 ds^+ - \iint_{x_2, x_3} f(x^-) \underline{n}^- \cdot \underline{e}_1 ds^-$$

$$= \iint_{x_2, x_3} f(x) \underline{n} \cdot \underline{e}_1 ds^*$$



Corollaire 1 : si  $f = f(x_1, x_2, x_3)$

$$\int_{\Omega} \left( \frac{\partial f}{\partial x_1} + \frac{\partial f}{\partial x_2} + \frac{\partial f}{\partial x_3} \right) dv = \int_{\partial \Omega} \left( f \underline{n} \cdot \underline{e}_1 + f \underline{n} \cdot \underline{e}_2 + f \underline{n} \cdot \underline{e}_3 \right) ds$$

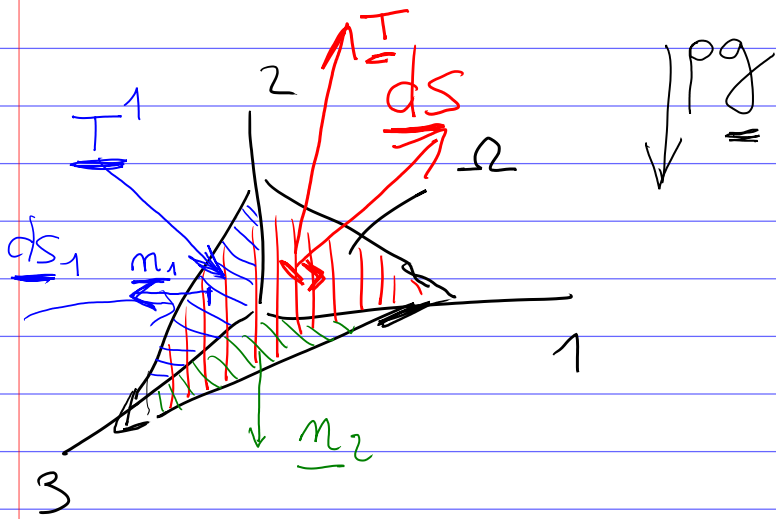
Corollaire 2 :

$$\text{Si } \underline{f} = \begin{pmatrix} f_1 \\ f_2 \\ f_3 \end{pmatrix} \quad \text{avec } f_k = f_k(x_1, x_2, x_3)$$

$$\begin{aligned} \int_{\Omega} \left( \frac{\partial f_1}{\partial x_1} + \frac{\partial f_2}{\partial x_2} + \frac{\partial f_3}{\partial x_3} \right) dv &= \int_{\partial\Omega} (f_1 n_1 + f_2 n_2 + f_3 n_3) ds \\ &= \int_{\partial\Omega} \underline{f} \cdot \underline{n} ds \end{aligned}$$

Classiquement "théorème de la divergence" :  $\int_{\Omega} \nabla \cdot \underline{f} dv = \int_{\partial\Omega} \underline{f} \cdot \underline{n} ds$   
↑  
div. (f)

# Retour : existence



A l'équilibre :  $\sum \vec{F} = 0$

$$ds_1 \times \underline{T}^1 + ds_2 \underline{T}^2 + ds_3 \underline{T}^3 + \underbrace{dx_1 dx_2 dx_3}_{\Omega} \underline{pg} = 0$$

3 premiers termes : forces de surface ( $\mathcal{O}(dx^2)$ )  
 dernier terme : force de volume ( $\mathcal{O}(dx^3)$ )

Dernier terme négligeable car  $\mathcal{O}(dx^3)$

$$\Rightarrow ds \left( \underline{n}_1 \cdot \underline{e}_1 \underline{T}^1 + \underline{n}_2 \cdot \underline{e}_2 \underline{T}^2 + \underline{n}_3 \cdot \underline{e}_3 \underline{T}^3 + \underline{T} \right) = 0$$

$$\Rightarrow ds \left( \underbrace{\underline{n}_1 \cdot \underline{e}_1}_{ds_1} \underline{T}^1 + \underline{n}_2 \cdot \underline{e}_2 \underline{T}^2 + \underline{n}_3 \cdot \underline{e}_3 \underline{T}^3 + \underline{T} \right) = 0$$

$$\Rightarrow \underline{T} = n_1 \underline{T}^1 + n_2 \underline{T}^2 + n_3 \underline{T}^3$$

$$\underline{T} = \begin{bmatrix} | & | & | \\ \underline{T}^1 & \underline{T}^2 & \underline{T}^3 \\ | & | & | \end{bmatrix} \times \begin{bmatrix} n_1 \\ n_2 \\ n_3 \end{bmatrix}$$

$(\underline{e}_1, \underline{e}_2, \underline{e}_3)$        $(e_1, e_2, e_3)$

$$ds_1 = ds \cdot \underline{e}_1$$

$$\underline{n}_1 = -\underline{e}_1$$

$$\underline{n}_2 = -\underline{e}_2$$

$$\underline{n}_3 = -\underline{e}_3$$

On vient de démontrer qu'il existe une application linéaire  $T_q$ .

$$\boxed{\underline{T}(\underline{x}, \underline{m}) = \underline{\underline{\sigma}}(\underline{x}) \cdot \underline{m}}$$

On appelle  $\underline{\underline{\sigma}}$  le tenseur des contraintes.

Notation : scalaire :  $\alpha$  (tenseur d'ordre 0)

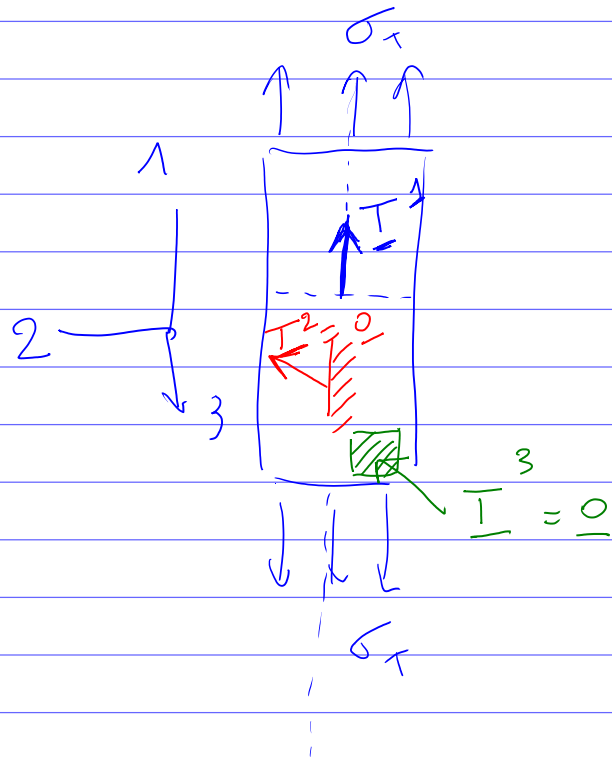
vecteur :  $\underline{\alpha}$  (ordre 1)

matrice :  $\underline{\underline{\alpha}}$  (ordre 2)

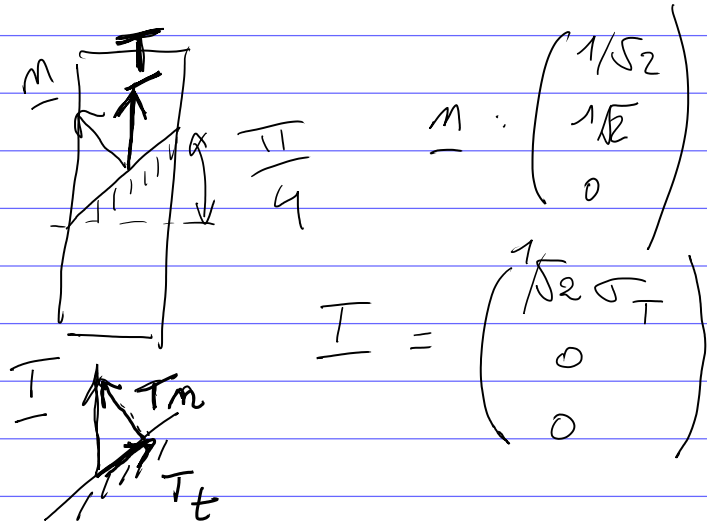
(tenseur d'ordre 3 :  $\underline{\underline{\underline{\alpha}}}$  ... ) ← aucune importance ici



\* Example



$$\sigma = \begin{pmatrix} \sigma_T & 0 & 0 \\ 0 & 0 & 0 \\ 0 & 0 & 0 \end{pmatrix}$$

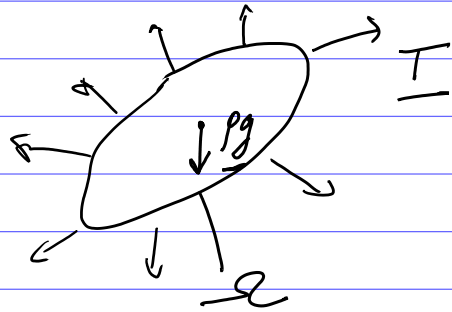


$$\sigma = \begin{pmatrix} 1/\sqrt{2} \\ 1/\sqrt{2} \\ 0 \end{pmatrix}$$

$$\tau = \begin{pmatrix} 1/\sqrt{2} \sigma_T \\ 0 \\ 0 \end{pmatrix}$$

## \* 2) Equilibre

1ère démonstration :



$$\int_{\underline{\Omega}} \underline{T} ds + \int_{\underline{\Omega}} \underline{\rho g} dv = 0$$

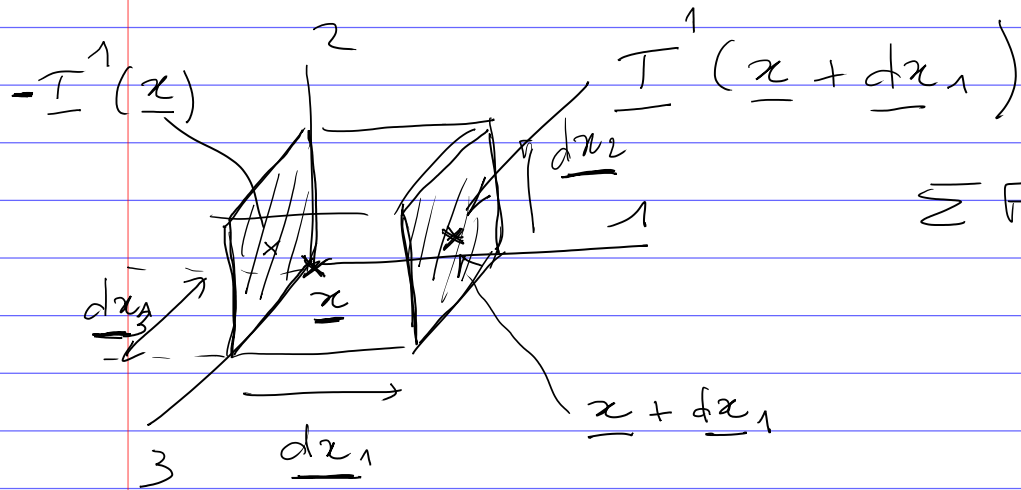
Th. de la divergence :  $\int_{\underline{\Omega}} \underline{T} ds = \int_{\underline{\Omega}} \underline{\underline{\sigma}} \underline{\underline{n}} ds = \int_{\underline{\Omega}} \nabla \cdot \underline{\underline{\sigma}} dv$

d'où  $\int_{\underline{\Omega}} (\nabla \cdot \underline{\underline{\sigma}} + \underline{\underline{\rho g}}) dv = 0 \quad \forall \underline{\Omega}$

donc  $\boxed{\nabla \cdot \underline{\underline{\sigma}} + \underline{\underline{\rho g}} = 0}$  Equ. d'équilibre

ou  $\nabla \cdot \underline{\underline{\sigma}} + \underline{\underline{\rho g}} = \underline{\underline{\rho \ddot{x}}}$  en dynamique

2ème démonstration :



$$\Sigma F = \left( \underline{T}^1(\underline{x} + d\underline{x}_1) - \underline{T}^1(\underline{x}) \right) \times d\underline{x}_2 d\underline{x}_3$$

$$+ \left( \underline{T}^2(\underline{x} + d\underline{x}_2) - \underline{T}^2(\underline{x}) \right) \times d\underline{x}_1 d\underline{x}_3$$

$$+ \left( \underline{T}^3(\underline{x} + d\underline{x}_3) - \underline{T}^3(\underline{x}) \right) \times d\underline{x}_1 d\underline{x}_2$$

$$+ d\underline{x}_1 d\underline{x}_2 + d\underline{x}_3 \rho \underline{g} = 0$$

↑  
équilibre

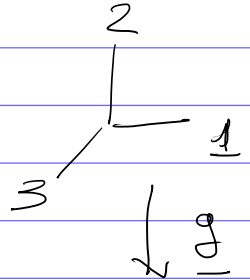
$$\frac{\Sigma F}{V} = \frac{\partial \underline{T}^1}{\partial x_1} + \frac{\partial \underline{T}^2}{\partial x_2} + \frac{\partial \underline{T}^3}{\partial x_3} + \rho \underline{g}$$

$$V = d\underline{x}_1 d\underline{x}_2 d\underline{x}_3$$

$$\Rightarrow \nabla \cdot \underline{\underline{\sigma}} + \rho \underline{g} = \underline{0}$$

$$\nabla \cdot \underline{v} = \frac{\partial v_1}{\partial x_1} + \frac{\partial v_2}{\partial x_2} + \frac{\partial v_3}{\partial x_3}$$

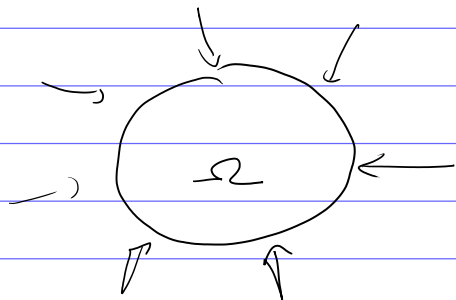
$$\nabla \cdot \underline{\underline{\sigma}} = \begin{pmatrix} \partial \sigma_{11} / \partial x_1 + \partial \sigma_{12} / \partial x_2 + \partial \sigma_{13} / \partial x_3 \\ \partial \sigma_{12} / \partial x_1 + \partial \sigma_{22} / \partial x_2 + \partial \sigma_{23} / \partial x_3 \\ \partial \sigma_{13} / \partial x_1 + \dots \end{pmatrix}$$



Exemple : fluide au repos

$$\underline{\underline{\sigma}} = \begin{pmatrix} -p & 0 & 0 \\ 0 & -p & 0 \\ 0 & 0 & -p \end{pmatrix}$$

$$\nabla \cdot \underline{\underline{\sigma}} = - \begin{pmatrix} \partial p / \partial x_1 \\ \partial p / \partial x_2 \\ \partial p / \partial x_3 \end{pmatrix} = - \underline{\underline{\rho g}} = - \rho \begin{pmatrix} 0 \\ -g \\ 0 \end{pmatrix} \Rightarrow p = -\rho g x_2 + \alpha$$



$$\int_{\partial\Omega} T ds = \int_{\Omega} \nabla \cdot \underline{\sigma} dv$$

$$\text{et si } \underline{\nabla \cdot \underline{\sigma}} = - \underline{\rho g}$$

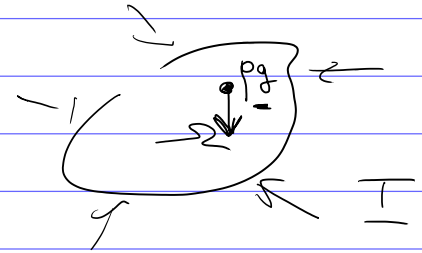
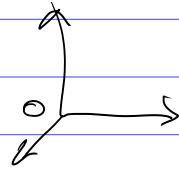
$$= \underline{\rho g} \int_{\Omega} dv = \underline{\rho g} V_{\Omega}$$

( poussée d'archimède )

### \* 3) Symmétrie

Somme des moments

$$\underline{M}_T = \int_{\partial \Omega} \underline{OM} \wedge \underline{T} \, ds, \quad \underline{M}_g = \int_{\partial \Omega} \underline{OM} \wedge \underline{pg} \, ds$$



$$\underline{M}_T = \int_{\partial \Omega} (\underline{OM} \wedge \underline{\sigma}) \cdot \underline{n} \, ds = \int_{\Omega} \nabla \cdot (\underline{OM} \wedge \underline{\sigma}) \, dV$$

$$\left( \underline{OM} \wedge \underline{\sigma} = \left( \begin{array}{c} \underline{OM} \wedge \underline{T}^1 \\ \underline{OM} \wedge \underline{T}^2 \\ \underline{OM} \wedge \underline{T}^3 \end{array} \right) \right)$$

$$\nabla \cdot (\underline{x} \wedge \underline{\sigma}) = ?$$

$$\frac{\partial (\underline{001} \wedge \underline{T}^{-1})}{\partial x_1} = \begin{pmatrix} 1 \\ 0 \\ 0 \end{pmatrix} \wedge \underline{T}^{-1} + \underline{x} \wedge \frac{\partial \underline{T}^{-1}}{\partial x_1}$$

$$= \begin{pmatrix} T_3^2 - T_2^3 \\ -T_3^1 + T_1^3 \\ T_2^1 - T_1^2 \end{pmatrix}$$

$$\nabla \cdot (\underline{x} \wedge \underline{\sigma}) = \begin{pmatrix} T_3^2 - T_2^3 \\ T_1^3 - T_3^1 \\ T_2^1 - T_1^2 \end{pmatrix} + \underline{x} \wedge \left( \frac{\partial T^1}{\partial x_1} + \frac{\partial T^2}{\partial x_2} + \frac{\partial T^3}{\partial x_3} \right) \begin{pmatrix} 1 \\ 0 \\ 0 \end{pmatrix} \wedge \underline{T}^{-1} = \begin{pmatrix} 0 \\ T_3^1 \\ -T_2^1 \end{pmatrix}$$

$$\frac{\partial}{\partial x_1} \begin{pmatrix} x_1 \\ x_2 \\ x_3 \end{pmatrix} = \begin{pmatrix} 1 \\ 0 \\ 0 \end{pmatrix}$$

$$\Rightarrow \underline{M}_t + \underline{M}_g = \int_{\Omega} \left[ \begin{pmatrix} T_3^2 - T_2^3 \\ \dots \\ \dots \end{pmatrix} + \underline{x} \wedge \left( \underline{\nabla} \cdot \underline{\sigma} + \underline{\rho g} \right) \right] dV$$

= 0 à l'équilibre

Vrai pour tout  $\Omega$  et pour tout choix de l'origine

↓  
donc le grand crochet  
a une intégrale nulle

↓  
Donc  $(\nabla \cdot \underline{\underline{\sigma}} + \underline{\underline{\rho g}}) = \underline{\underline{0}}$

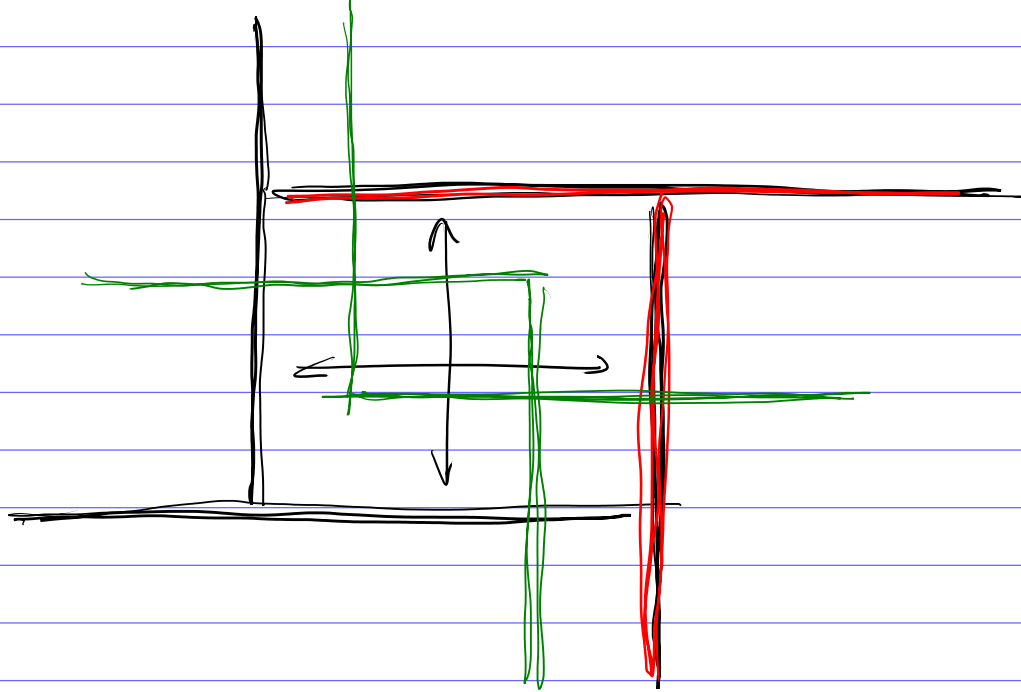
↙ ↘  
donc  $\begin{pmatrix} T_3^2 - T_2^3 \\ \dots \\ \dots \end{pmatrix} = \underline{\underline{0}}$

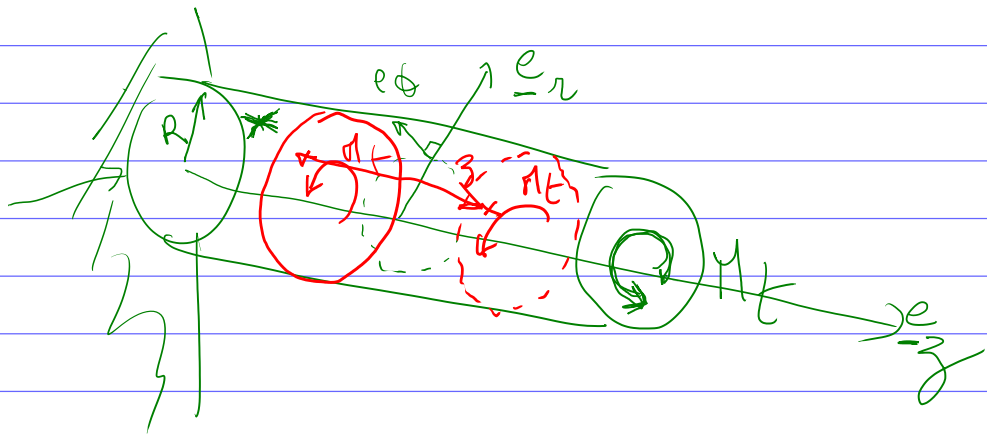
i.e.  $\sigma_{12} = \sigma_{21}$

$$\sigma_{13} = \sigma_{31}$$

$$\sigma_{23} = \sigma_{32}$$







1) Ecrire l'équation d'éq.

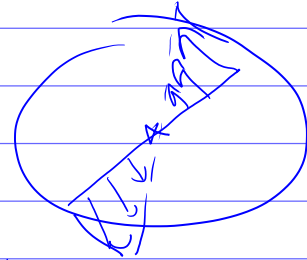
$$\nabla \cdot \underline{\underline{\sigma}} + \rho \underline{\underline{g}} = \underline{\underline{0}}$$

2) Conditions aux limites : en tout point de  $\partial\Omega$   
dire ce qui est imposé

i.e. :  $\underline{\underline{\sigma}} \cdot \underline{\underline{n}} = \underline{\underline{T}}_{\text{imposé}}$  sur tout  $\partial\Omega$

exemple : en  $r=R$   $\underline{\underline{\sigma}} \cdot \underline{\underline{e}}_r = \begin{pmatrix} 0 \\ 0 \\ 0 \end{pmatrix}$   $\leftarrow$  C.L. "air libre"

3) Rappel de RDM  
en torsion

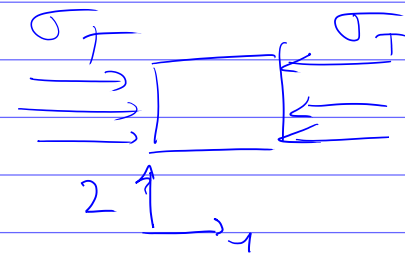


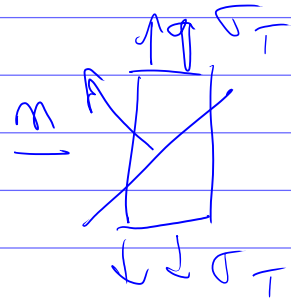
$$\underline{\underline{\tau = \alpha \theta_t r e_\theta}}$$

Comment faire un  $\underline{\underline{\sigma}}$  sur une surface  $\perp e_z$   
avec ça et est-ce que il satisfait  
eq. d'équilibre<sup>(1)</sup> et conditions aux limites<sup>(2)</sup>?

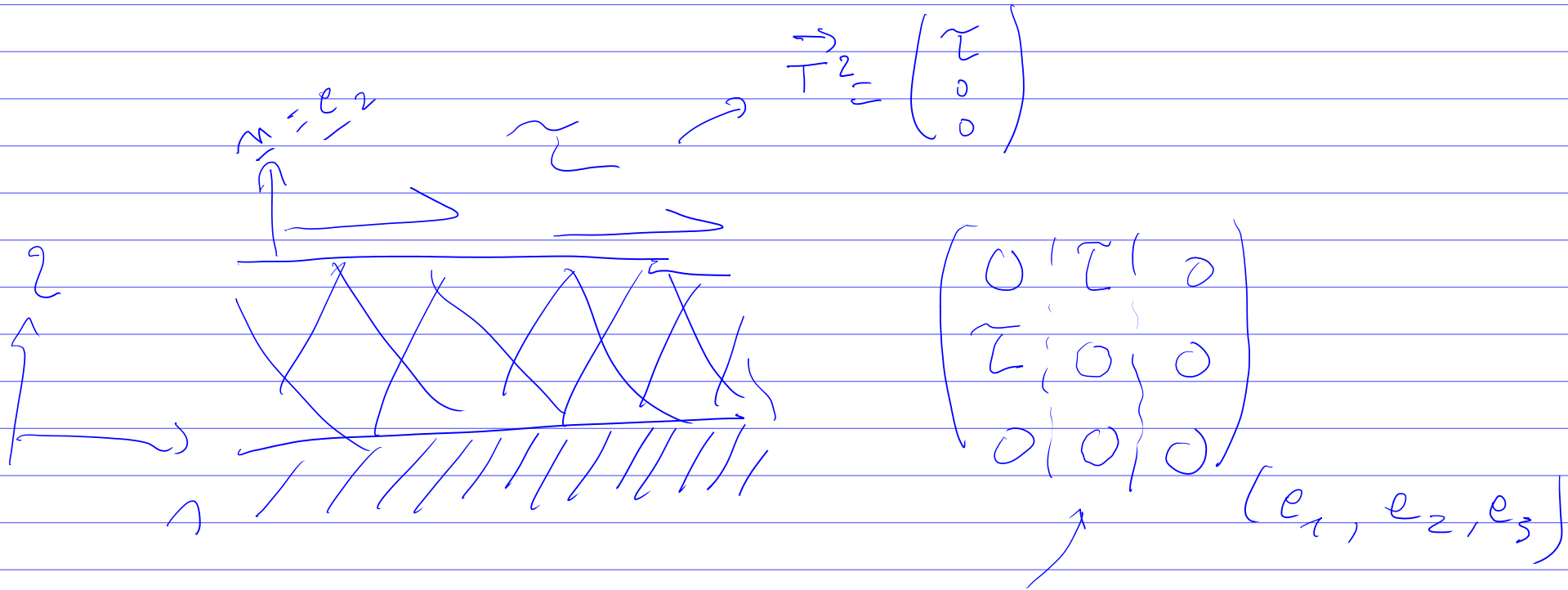
QCM fin de séance  
porte sur séance précédente

( QCM 1 = contraintes )

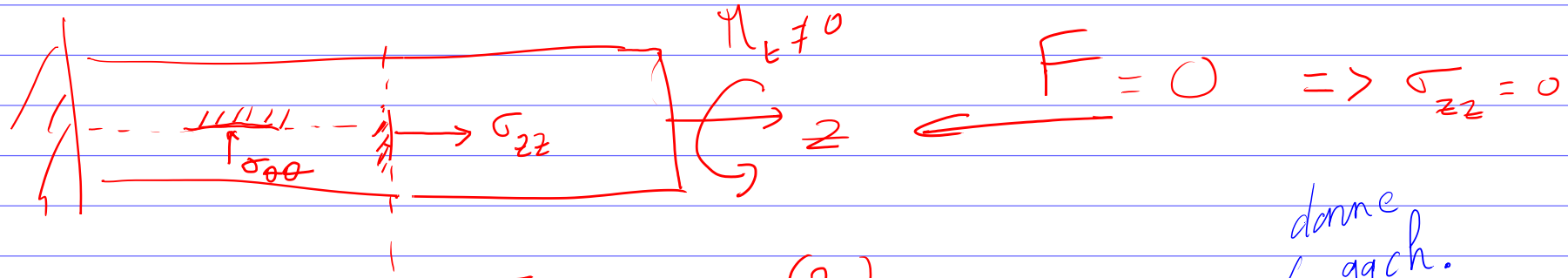
Ex de question :  que vaut  $\sigma_n$ ?



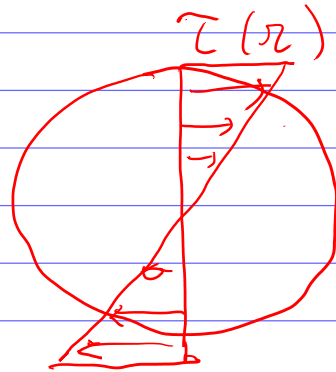
que vaut  $\tau(\alpha)$ ?



Cisaillement pur



$$\sigma_{zz} = 0 \quad (?)$$



$$T(r, e_z) = \underline{\tau} = \alpha r e_z \quad \forall \sigma$$

donne qqch. dans

